

# Nonlinear port-Hamiltonian modeling and simulation of rigid body and multibody system dynamics

Lisa Latussek | Master thesis (2025)

## Motivation

### Objective:

Complex multibody systems (MBS) need robust models that handle large rotations, conserve energy, and remain modular.

### Approach:

- Director formulation + port-Hamiltonian (PH) framework
  - Singularity-free description of rotations, constant mass matrix, energy consistency, and modular structure.
- Classical kinematic pairs linked to PH interconnections.
- Structure-preserving discretization ensures correct energy and angular momentum balances and avoids drift.

## Director formulation [1]

### Kinematics:

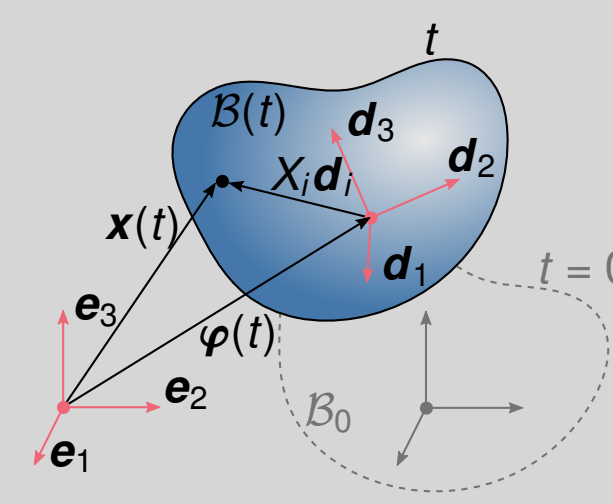
$$\mathbf{x}(X, t) = \boldsymbol{\varphi}(t) + X_i \mathbf{d}_i(t)$$

- Rigid body configuration in 12 redundant coordinates:

$$\mathbf{q} = (\boldsymbol{\varphi}, \mathbf{d}_1, \mathbf{d}_2, \mathbf{d}_3)$$

- Holonomic orthonormality constraints:

$$\mathbf{g}_\alpha(\mathbf{q}) = \begin{bmatrix} \frac{1}{2}(\mathbf{d}_1^T \mathbf{d}_1 - 1) \\ \frac{1}{2}(\mathbf{d}_2^T \mathbf{d}_2 - 1) \\ \frac{1}{2}(\mathbf{d}_3^T \mathbf{d}_3 - 1) \\ \mathbf{d}_1^T \mathbf{d}_2 \\ \mathbf{d}_1^T \mathbf{d}_3 \\ \mathbf{d}_2^T \mathbf{d}_3 \end{bmatrix} = \mathbf{0}$$



## PH systems

- State variables:  $\mathbf{x} = (\mathbf{q}, \mathbf{v}, \boldsymbol{\lambda})$

- PH-DAE formulation, cf. [2]:

$$\mathbf{E}\dot{\mathbf{x}} = \mathbf{J}(\mathbf{x})\mathbf{z}(\mathbf{x}) + \mathbf{B}(\mathbf{x})\mathbf{u} \quad \text{and} \quad \mathbf{E}^T\mathbf{z}(\mathbf{x}) = \nabla H(\mathbf{x})$$

$$\mathbf{y} = \mathbf{B}^T(\mathbf{x})\mathbf{z}(\mathbf{x})$$

- $\mathbf{J}(\mathbf{x}) = -\mathbf{J}(\mathbf{x})^T$  encodes (nonlinear) interconnection
- Power balance equation:

$$\frac{d}{dt} H = \nabla H(\mathbf{x})^T \dot{\mathbf{x}} = \mathbf{z}^T \mathbf{E}\dot{\mathbf{x}} = \mathbf{z}^T \mathbf{B}\mathbf{u} = \mathbf{y}^T \mathbf{u}$$

- For interconnection, decomposition internal and external ports for  $\alpha \in \{A, B\}$ , cf. [3]:

$$\mathbf{B}^\alpha \mathbf{u}^\alpha = \begin{bmatrix} \mathbf{B}_{\text{int}}^\alpha & \mathbf{B}_{\text{ext}}^\alpha \end{bmatrix} \begin{bmatrix} \mathbf{u}_{\text{int}}^\alpha \\ \mathbf{u}_{\text{ext}}^\alpha \end{bmatrix}$$

## Contributions

### PH formulation

- PH-DAE formulation for a rigid body:

$$\begin{bmatrix} \mathbf{I} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{M} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} \end{bmatrix} \begin{bmatrix} \dot{\mathbf{q}} \\ \dot{\mathbf{v}} \\ \dot{\boldsymbol{\lambda}} \end{bmatrix} = \begin{bmatrix} \mathbf{I} & \mathbf{0} & \mathbf{0} \\ -\mathbf{I} & \mathbf{0} & -\nabla \mathbf{g}(\mathbf{q})^T \\ \mathbf{0} & \nabla \mathbf{g}(\mathbf{q}) & \mathbf{0} \end{bmatrix} \begin{bmatrix} \nabla V(\mathbf{q}) \\ \mathbf{v} \\ \boldsymbol{\lambda} \end{bmatrix} + \mathbf{B}(\mathbf{x})\mathbf{u}$$

- Transformer interconnection for joints:

$$\begin{bmatrix} \mathbf{y}_{\text{int}}^A \\ \mathbf{u}_{\text{int}}^A \end{bmatrix} = \begin{bmatrix} \mathbf{0} & \mathbf{I} \\ -\mathbf{I} & \mathbf{0} \end{bmatrix} \begin{bmatrix} \mathbf{u}_{\text{int}}^B \\ \mathbf{y}_{\text{int}}^B \end{bmatrix}$$

- PH-DAE dynamics of two interconnected bodies:

$$\begin{bmatrix} \mathbf{E}^A & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{E}^B & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} \end{bmatrix} \begin{bmatrix} \dot{\mathbf{x}}^A \\ \dot{\mathbf{x}}^B \\ \dot{\boldsymbol{\lambda}}_J \end{bmatrix} = \begin{bmatrix} \mathbf{J}^A & \mathbf{0} & \mathbf{B}_{\text{int}}^A \\ \mathbf{0} & \mathbf{J}^B & -\mathbf{B}_{\text{int}}^B \\ -(\mathbf{B}_{\text{int}}^A)^T & (\mathbf{B}_{\text{int}}^B)^T & \mathbf{0} \end{bmatrix} \begin{bmatrix} \mathbf{z}^A \\ \mathbf{z}^B \\ \boldsymbol{\lambda}_J \end{bmatrix} + \mathbf{B}_{\text{ext}} \mathbf{u}_{\text{ext}}$$

### Link to kinematic pairs

- PH interconnection contains exact same information as kinematic pair for ideal constraints
- Analogy provides rigorous link between PHS from systems theory and classical multibody dynamics
- Definition velocity-related port matrix  $\tilde{\mathbf{B}}^\alpha(\mathbf{x})$ :

$$\mathbf{B}^\alpha(\mathbf{x})\mathbf{u} = \begin{bmatrix} \mathbf{0} \\ \tilde{\mathbf{B}}^\alpha(\mathbf{x}) \\ \mathbf{0} \end{bmatrix} \mathbf{u}$$

- Key observation:

$$\begin{bmatrix} -(\tilde{\mathbf{B}}_{\text{int}}^A)^T & (\tilde{\mathbf{B}}_{\text{int}}^B)^T \end{bmatrix} \begin{bmatrix} \mathbf{v}^A \\ \mathbf{v}^B \end{bmatrix} = \nabla \mathbf{g}_J(\mathbf{q}) \mathbf{v}$$

### Time integration

- One-step implicit midpoint rule with  $\mathbf{x}^{n+\frac{1}{2}} = \frac{1}{2}(\mathbf{x}^{n+1} + \mathbf{x}^n)$ 
  - 2nd-order accurate
  - Consistent energy and angular momentum balances
  - Position level constraints satisfied

- Time-discrete update equations:

$$\mathbf{E}(\mathbf{x}^{n+1} - \mathbf{x}^n) = h \mathbf{J}(\mathbf{x}^{n+\frac{1}{2}}) \mathbf{z}^{n+\frac{1}{2}} + h \mathbf{B}(\mathbf{x}^{n+\frac{1}{2}}) \mathbf{u}^{n+\frac{1}{2}}$$

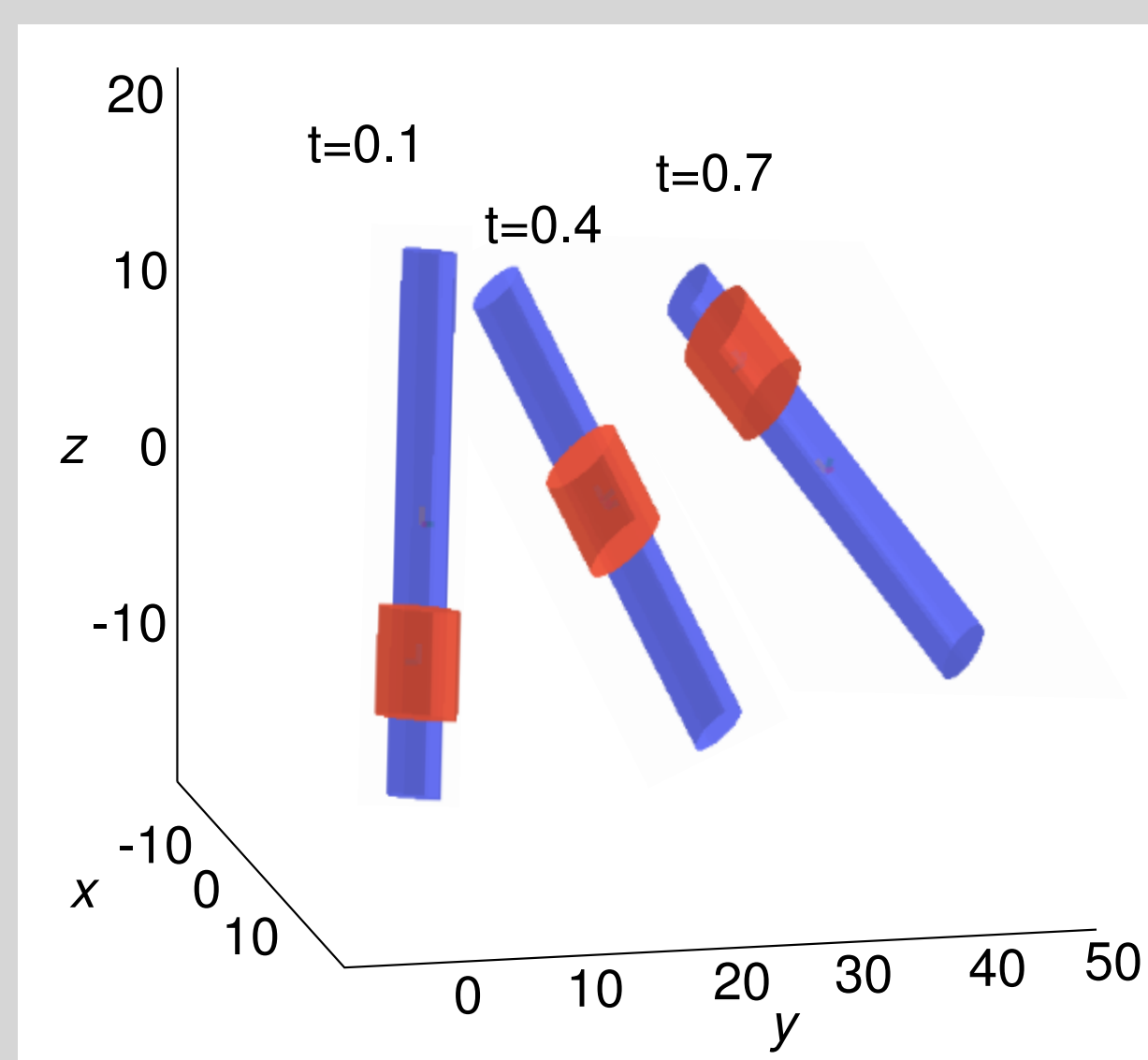
$$\mathbf{E}^T \mathbf{z}^{n+\frac{1}{2}} = \nabla H(\mathbf{x}^{n+\frac{1}{2}})$$

$$\mathbf{y}^{n+\frac{1}{2}} = \mathbf{B}(\mathbf{x}^{n+\frac{1}{2}})^T \mathbf{z}^{n+\frac{1}{2}}$$

- Consistent discrete-time power balance:

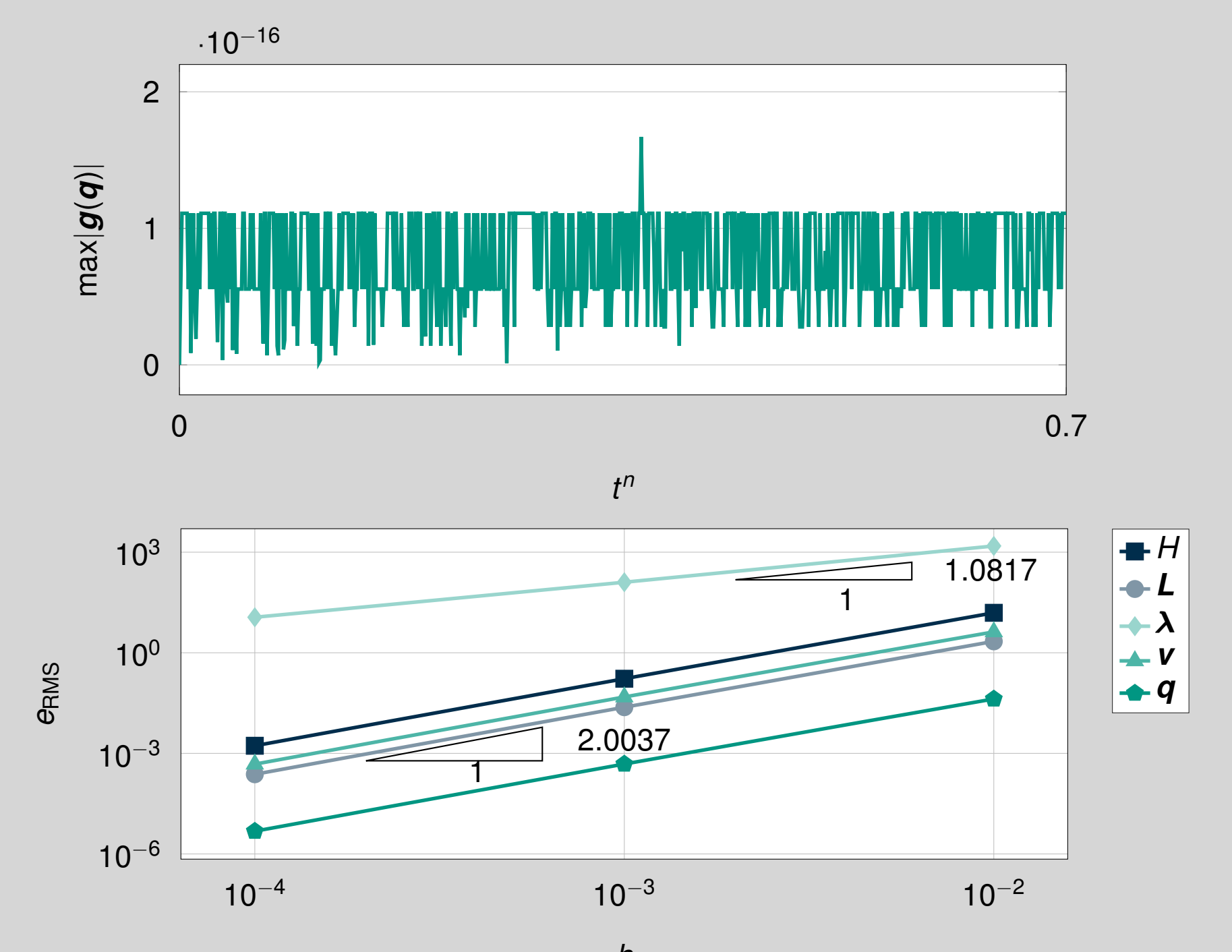
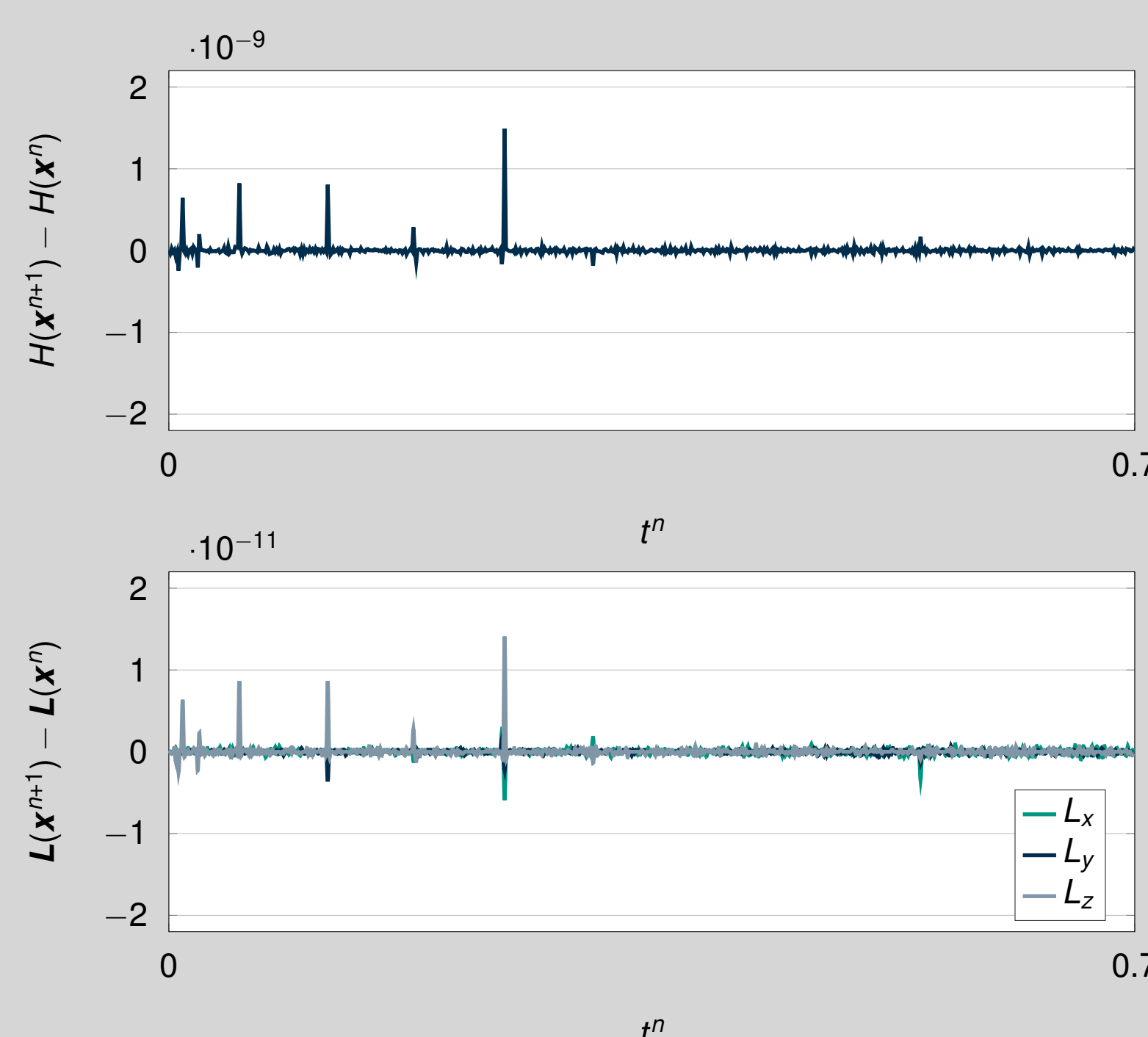
$$H(\mathbf{x}^{n+1}) - H(\mathbf{x}^n) = h (\mathbf{y}^{n+\frac{1}{2}})^T \mathbf{u}^{n+\frac{1}{2}}$$

## Numerical example [4]



Flying cylindrical pair

## Properties



## References

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